

The effect of atmospheric instability on wave growth

National Marine Environmental Forecasting Center

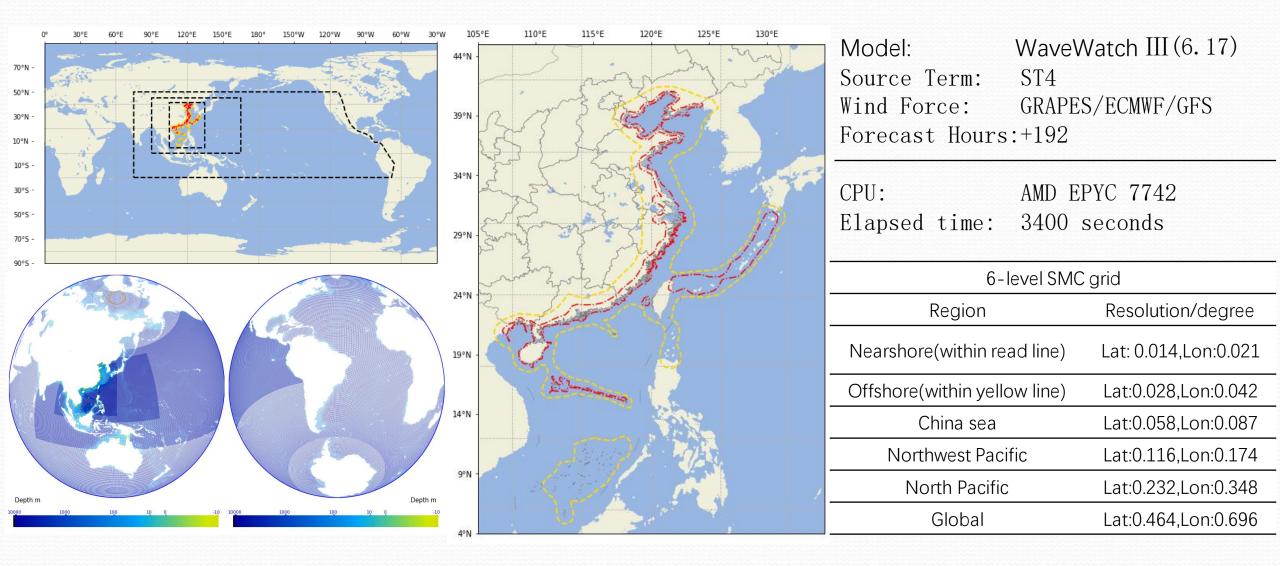
Fang Hou, Rui Xu

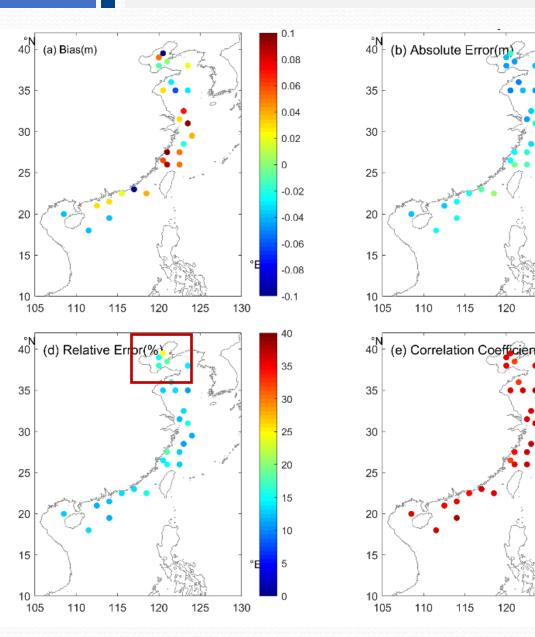
gblq@2216@163.com April 12th, 2024

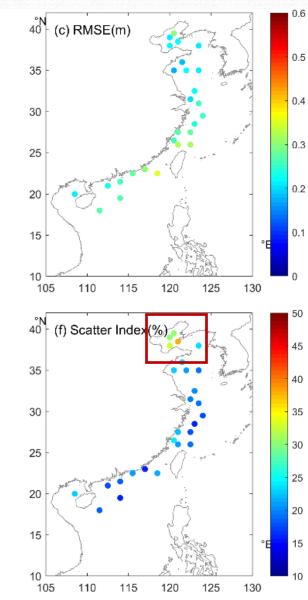
Outline

- Research purpose
- Background
- Methodology
- Results and Discussion

Motivation







0.5

0.45

0.4

0.35

0.3

0.2

0.15

0.1

0.05

0.95

0.9

0.85

0.8

0.7

0.65

0.6

0.55 0.5

0

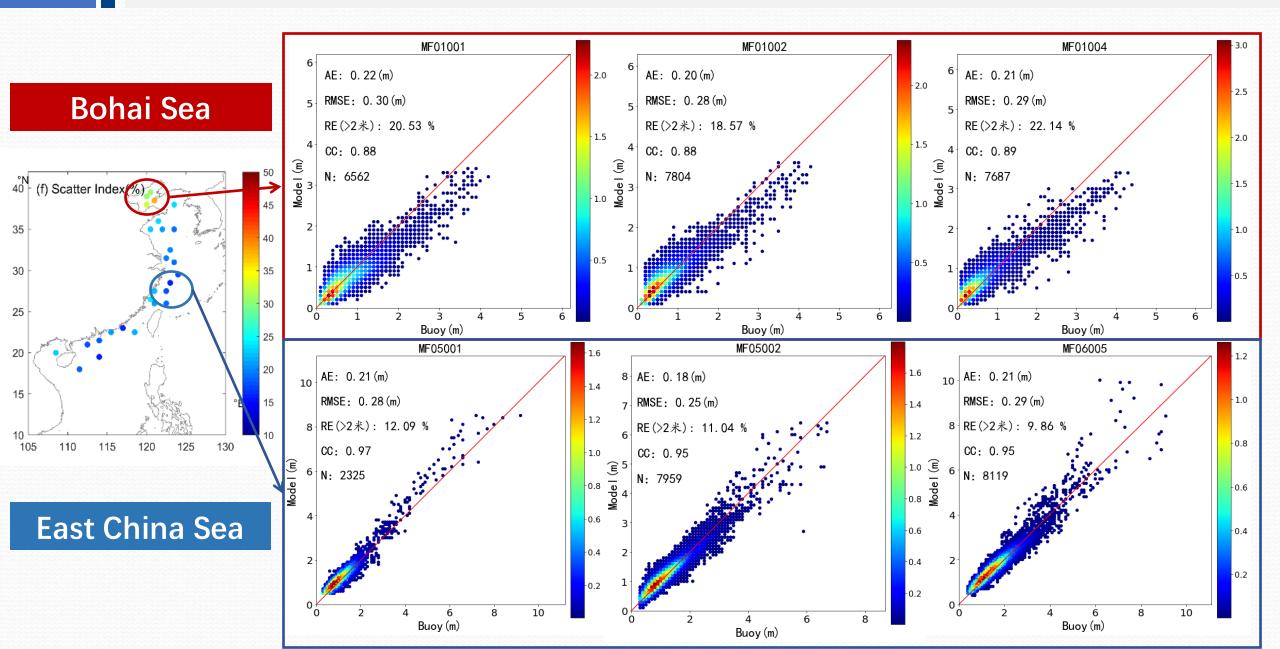
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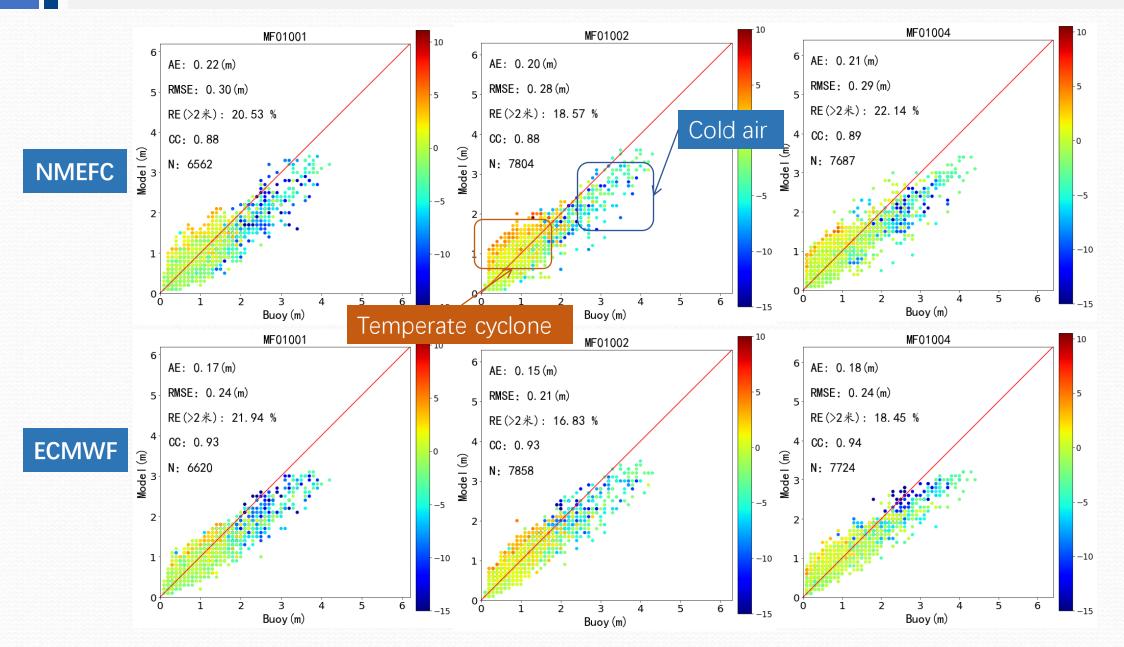
125

130

130

our model performed not well in Bohai and Yellow Sea , and that can be seen from relative error and scatter index





ST4 Parameterization scheme $S_{in}(k,\theta) = \frac{\rho_a}{\rho_w} \frac{\beta_{\max}}{\kappa^2} e^Z Z^4 \left(\frac{u_*}{C} + z_\alpha\right)^2 \cos^{Pin}(\theta - \theta_u) \sigma N(k,\theta) + S_{out}(k,\theta)$ $Z = \log(kz_1) + \kappa / [\cos(\theta - \theta_u)(u_*/C + z_\alpha)]$ $z_1 = \alpha_0 \frac{\tau}{1 - \tau_w / \tau}$ It seems that atmospheric instability was not taken into $U_{10} = \frac{u_*}{\kappa} \log \left(\frac{z_u}{z_1}\right)$ account when calculating the friction velocity.

 u_* Friction velocity is a const turbulent velocity scale that controls momentum transport within the z-altitude layer

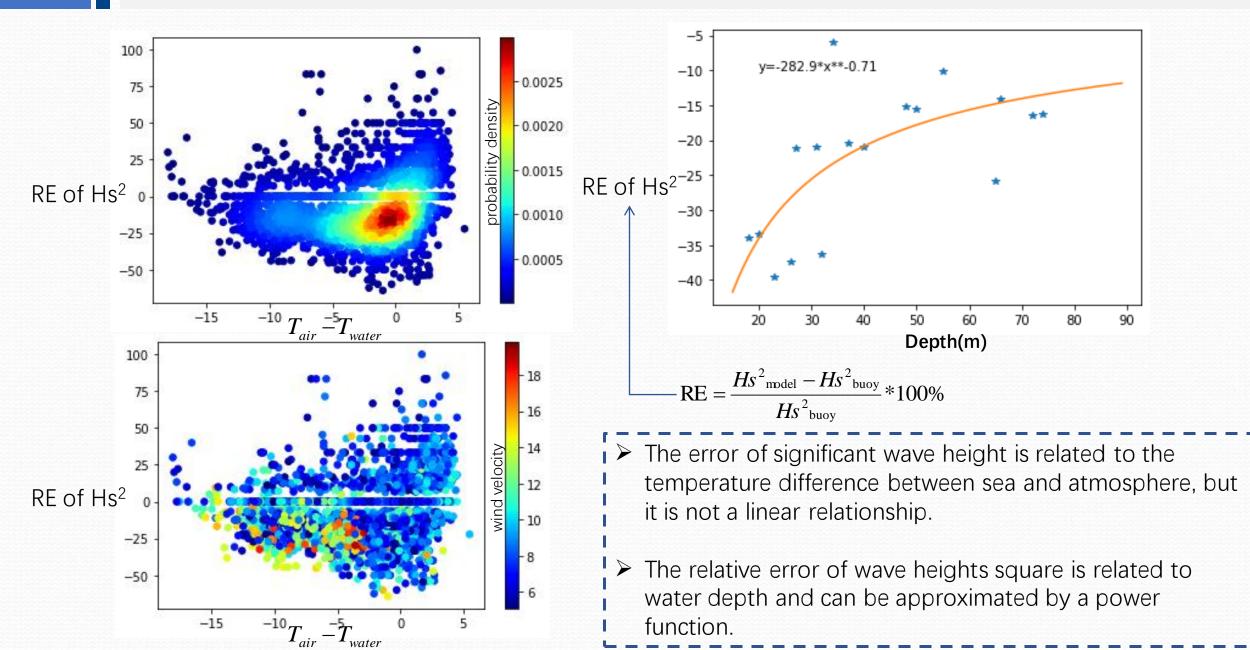
The calculation of friction velocity is based on the assumption of **Constant Flux Layer**, which overly simplifies the physical process of the air sea interface.

Factors such as **wave steepness**, **wave breaking**, **gusts**, **spectral width**, **and swell** can all affect the calculation of friction velocity, and friction velocity does not seem to be an isotropic constant.(Ortiz-Suslow,2021;Mahrt et al.,2018;(Kudryavtsev and Makin,2004;Chia-Huan Ting,2012)

| | Methodology | Effect | Comparison of Friction velocity from Coare an FLx4 | |
|---|---|--|--|--|
| ST4 (STAB3) | Parameterization considering gust effects | Maybe improved result for high wind speeds | 0.0025 Cd_COARE Cd_flx4 0.0020 | |
| ST2 (STAB2) | Parameterization considering stability correction | Improved underestimation of ST2 | 0.0015 - | |
| COARE3.5 | A comprehensive model for calculating wind stress | Inconsistent with the friction wind speed in the model | 0.0010 - 0.0005 - | |
| Young, 1998 | Correction formula fitted from observations | The correction effect is not ideal, especially under high wind speeds | $0.0000 \underbrace{\begin{array}{c} 0.0000 \\ 0.0 \end{array}}_{0.0 2.5 5.0 7.5 10.0 12.5 15.0 17.5 20.0}$ | |
| In general, although various methods take atmospheric instability into account in different forms to calculate or correct u*, there has been no improvement in forecast accuracy in the Bohai Sea region in practical | | | coefficient of correction from Young(1998) $R_{b} = \frac{g(T_{a} - T_{w})}{z_{t}T_{a}(\frac{u}{z})^{2}}$ | |

 $\xi = -1.22R_{b} + 0.01$

account in different forms to calculate or correct u*, there has been no improvement in forecast accuracy in the Bohai Sea region in practical applications.



$$\xi = C_1 * U_{10}^{C_2} * Sign(T_{2m} - SST) * (T_{2m} - SST) + C_3)^{C_4} + C_5$$

$$u_* = u_* * \xi; \quad Hs_{buoy} = Hs_{mod \, el} * \xi$$

$$u_* = r_* * \xi; \quad Hs_{buoy} = Hs_{mod \, el} * \xi$$

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$$(1) Depth < 50 (m) \&$$

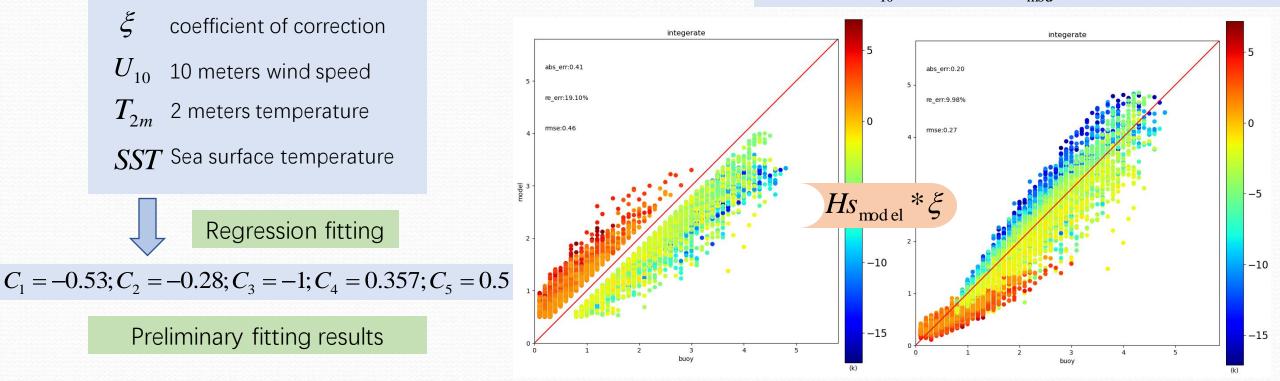
$$(2) Hs_{mod} > 0.3 \&$$

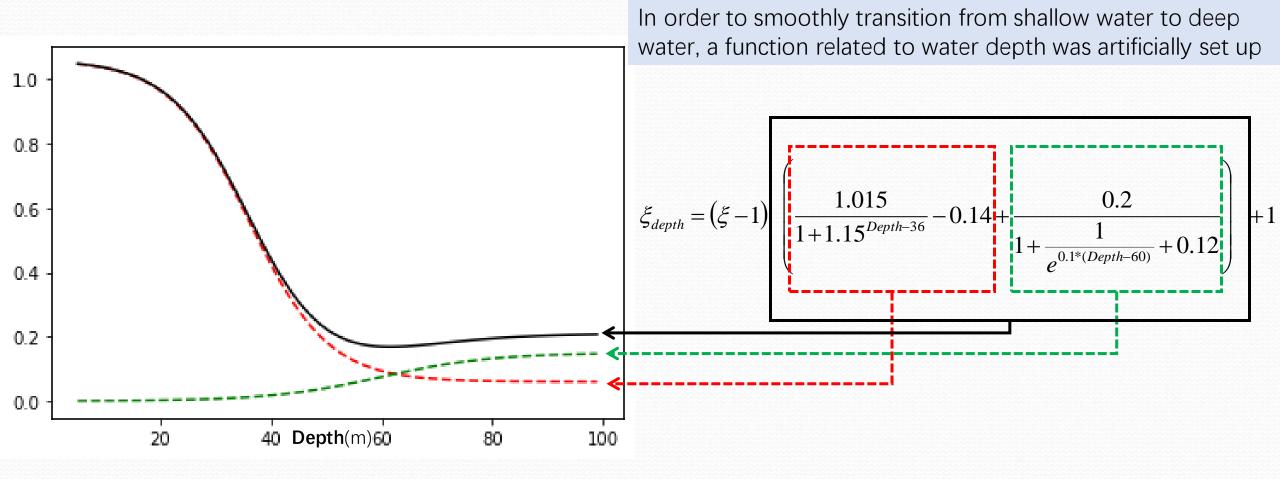
$$(3) Hs_{mod} - Hs_{buoy} < -0.2 \& T_{2m} - SST < 0 \&$$

$$(4) Hs_{mod} - Hs_{buoy} > 0.2 \& T_{2m} - SST > 0 \&$$

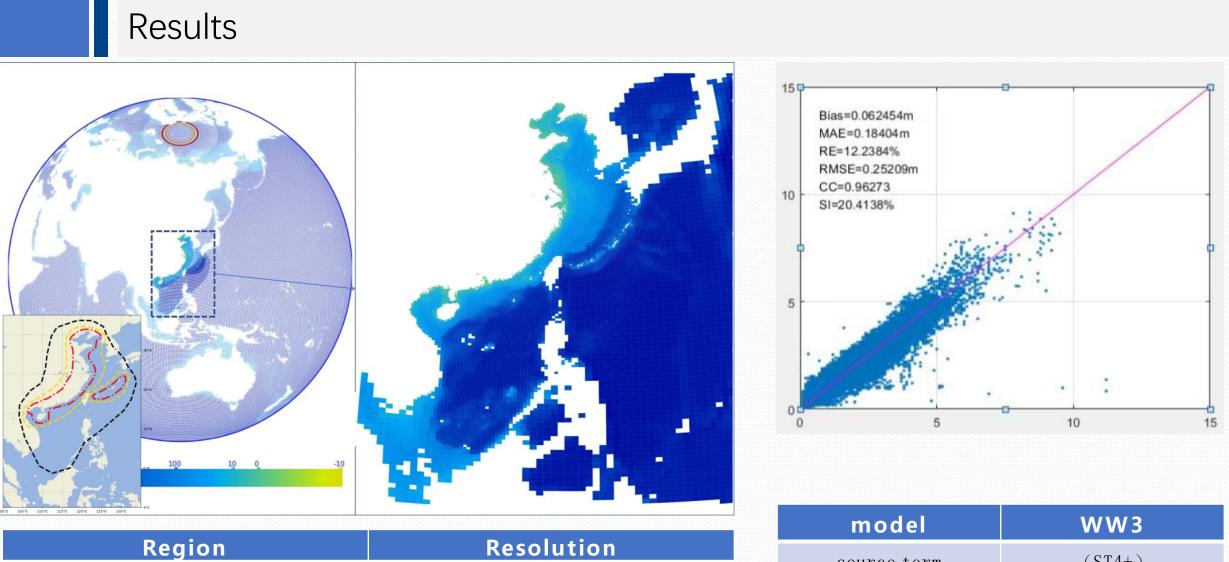
$$(5) . not . (U_{10} < 8 \& Hs_{mod} > 2.5) \&$$

$$(6) . not . (U_{10} > 12 \& Hs_{mod} < 0.8)$$





Assumption: The impact of atmospheric instability gradually decreases as water depth increases.



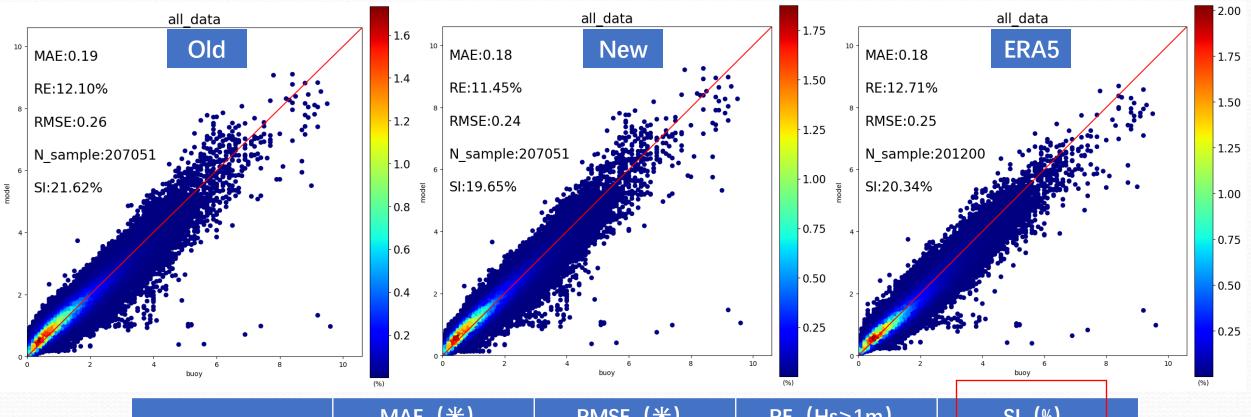
| Within the red line range |
|---------------------------------------|
| Within the yellow line range |
| Within the black line range |
| Global (Outside the black line range) |

| Re | SO | lut | ion | |
|----|-----|-----|--------|---|
| 1 | • • | 007 | (a la | _ |

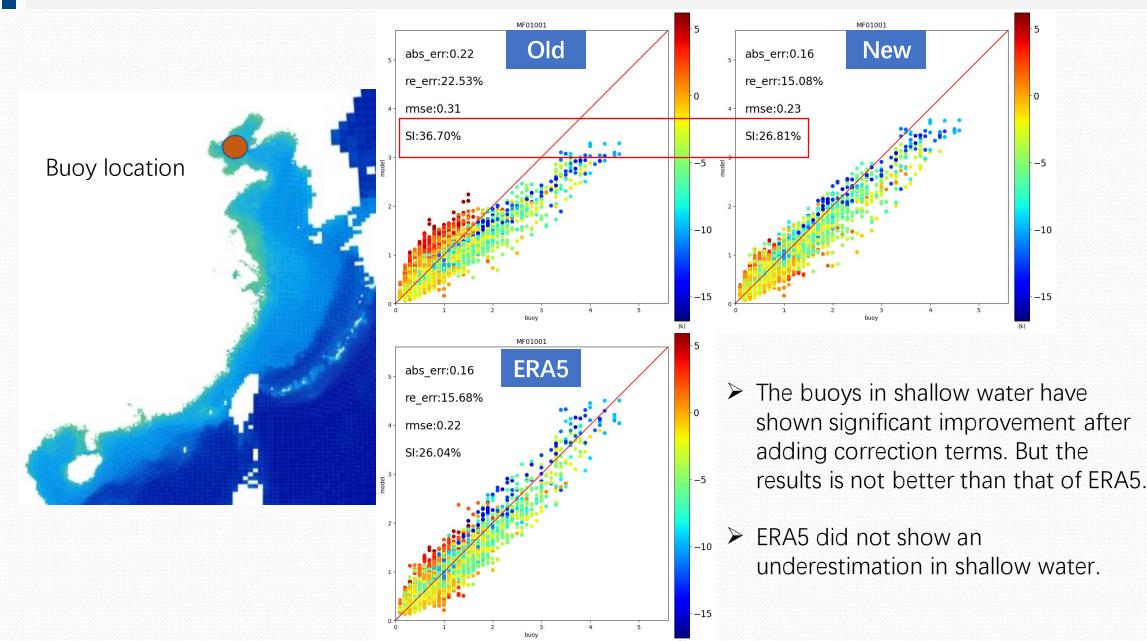
| lat:0.058, lon:0.087 | (about 6km) |
|----------------------|-------------|
| lat:0.116,1or | n:0.174 |
| lat:0.232,1or | n:0.348 |
| lat:0.464,lor | n:0.696 |

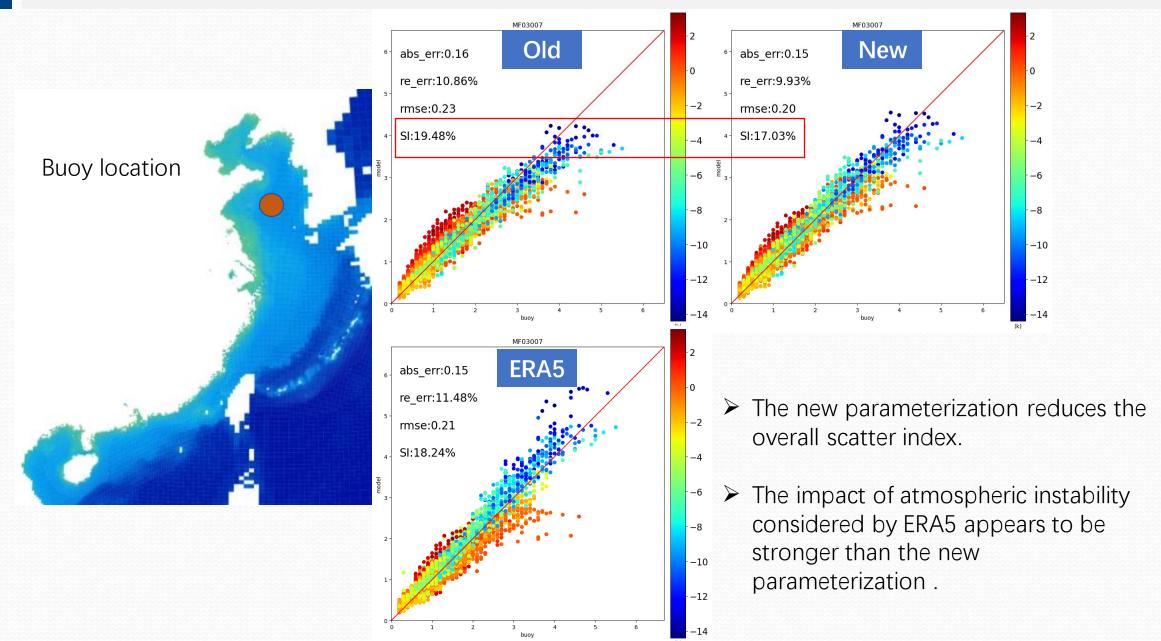
| model | WW3 | | |
|-----------------|-----------------------|--|--|
| source term | (ST4+) | | |
| force wind | ERA (u10, v10,2t,sst) | | |
| time span | 2021 | | |
| time resolution | Hourly | | |

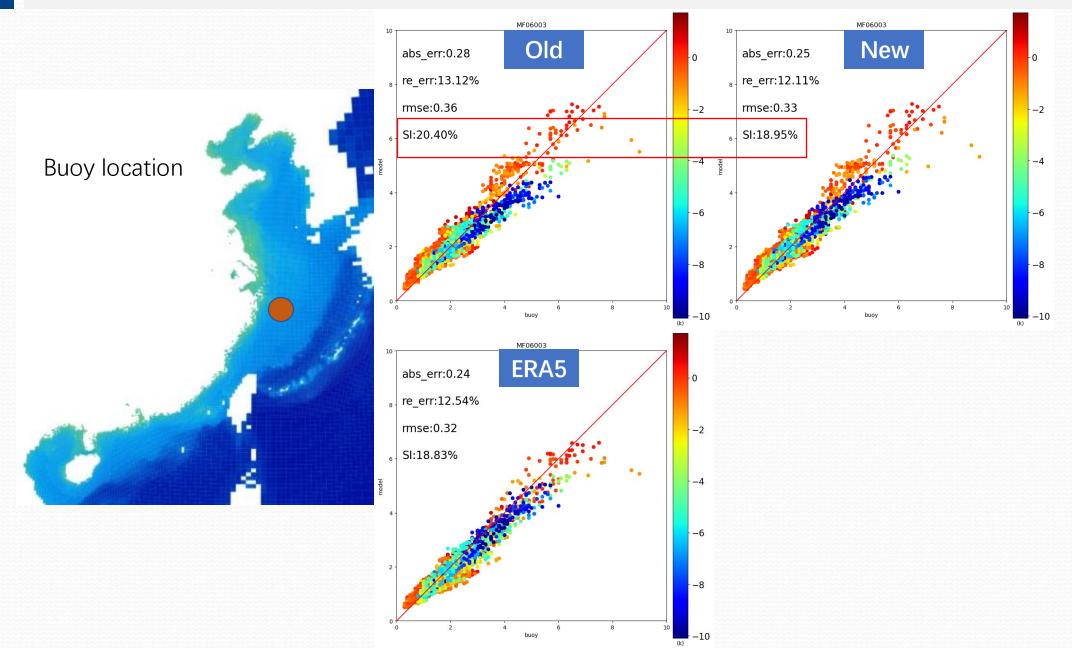
We used ERA5's 10 meters wind, 2 meters temperature, and sea surface temperature to calculate the hindcast Hs for 2021 No assimilation or fusion of observed data. Removed buoys that are too close to the shore

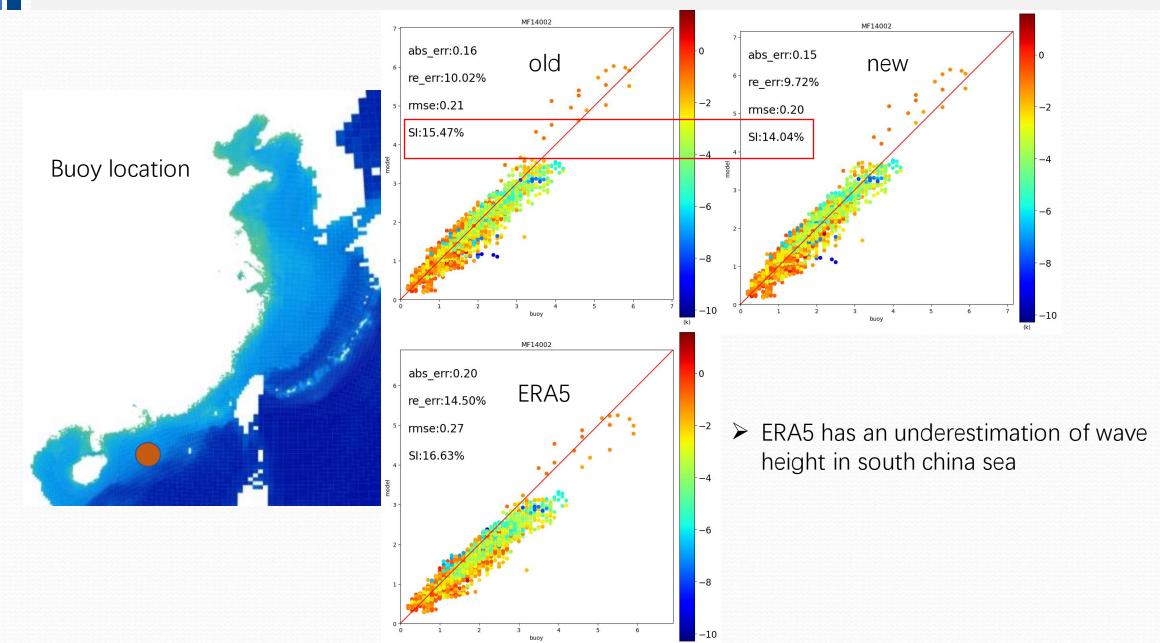


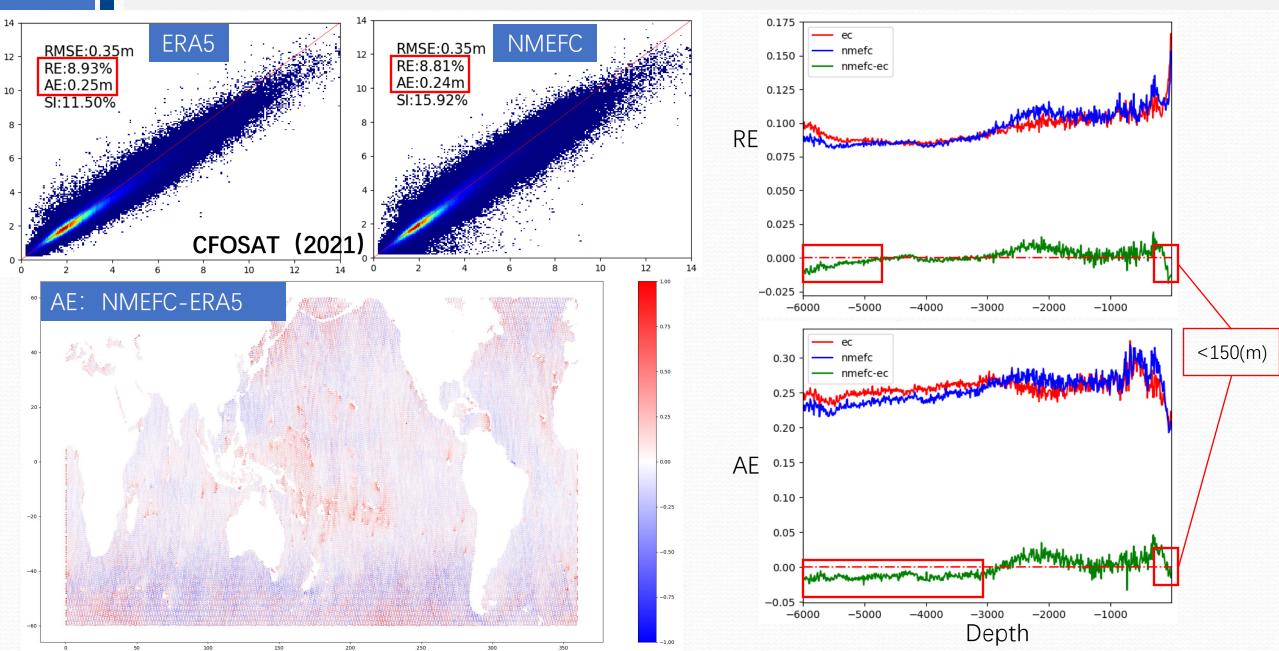
| | MAE(米) | RMSE(米) | RE (Hs>1m) | SI (%) | |
|-------------|--------|---------|------------|--------|--|
| NMEFC (old) | 0.19 | 0.26 | 12.10% | 21.62 | |
| NMEFC(new) | 0.18 | 0.24 | 11.45% | 19.65 | |
| ERA5 | 0.18 | 0.25 | 12.71% | 20.34 | |



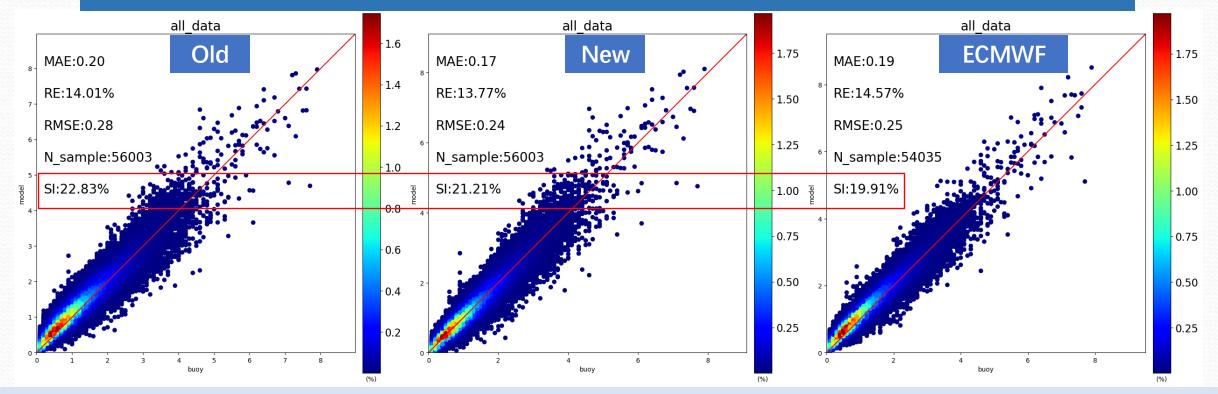








The application of the new parameterization to the forecasting model



We used ECMWF's(0.4 degrees)forecasting u10,v10,2t,skt to calculate the Hs for 2023

> The parameterization which performed well in hindcasting model is not applicable to forecasting model.

- We have adjusted the parameters again, but the SI is still higher than ecmwf.(may be caused by the low resolution of the wind)
- > Compared to the origional parameterization , there is still an overall improvement

Summary

- Compared to ST4, the new parameterization has made overall improvements in both hindcasting and forecasting.
- The physical meaning behind the new parameterization is very ambiguous. This new parameterization scheme should only be a transitional method, and formulas based on the new boundary layer theories should be the correct solution
- There are subtle differences in the wind field between ERA5 and ECMWF's forecasting data, and thus the same parameterization cannot be directly applied to both.

Plan for the Next Step

- > Further adjust the parameterization to make it more suitable for the forecasting model.
- > Consider utilizing machine learning for parameters regression and fitting
- > Apply for joining the (LC-WFV) project.

Thanks!